

DAMAGE ASSESSMENT ON ROAD STRUCTURES DUE TO SLOPE FAILURES IN THE 2011 OFF THE PACIFIC COAST OF TOHOKU EARTHQUAKE

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ABSTRACT: The damage on road structures due to slope failures in the 2011 off the Pacific Coast of Tohoku earthquake is assessed. We classify 13 types of failure modes for 43 data and analyze them from view of points of dependency of the damage on spatial distributions of peak ground acceleration, peak ground velocity, and seismic intensity induced by the earthquake. Previously proposed damage functions on the failures of road structures due to slope failures in the 2008 Iwate-Miyagi Nairiku earthquake are verified by comparing the derived results with the values from the damage functions.

Key Words: The 2011 off the Pacific Coast of Tohoku earthquake, the 2008 Iwate-Miyagi Nairiku earthquake, slope failure, road structure, damage function

INTRODUCTION

Road structures were damaged severely in the 2011 off the Pacific Coast of Tohoku earthquake ($M_{JMA}=9.0$) (JMA 2011a) due to not only tsunami waves, but also induced ground excitations. The ground excitations caused the slope failures in mountainous areas which induce various types of damage of road structures. The related researchers and practitioners paid intended attention to the damage of infrastructures such as road structures due to slope failures during strong ground excitations in previous extreme earthquakes such as the 2008 Iwate-Miyagi Nairiku earthquake ($M_{JMA}=7.2$) (Joint Survey Team of JSCE, JGS, JAEE, and the Japan Landslide Society 2008) and the 2008 Wenchuan earthquake, China ($M_w=7.9$) (USGS 2008) (Chigira 2005, Hunag et al. 2007, Nishida et al. 2007, Fujiwara et al. 2008, Tamakoshi 2008, Kokusho et al. 2009, Konagai et al. 2009, Nishiki et al. 2009, and Zhang et al. 2009). In these earthquakes, pavement of road structures were suffered and cut slopes of road structures were collapsed due to slope failures by ground shakings. Previous studies were involved in clarifying mechanism of occurrence of slope failures during an earthquake and in

Table 1 Analyzed data of damaged road structures

Road Management Sectors	Damage Information (URL)	Road Management Sectors	Damage Information (URL)
Tohoku Regional Development Bureau Main Office	【Disaster Prevention Information】(Press Release) Tohoku Regional Development Bureau Earthquake Information (15th Version) http://www.thr.mlit.go.jp/bumon/kisya/saigai/sback/zokuhou1110.htm	Kanto Regional Development Bureau Omiya National Road Office	Road Damage Information in the 2011 off the Pacific Coast of Tohoku Earthquake (1st and 3rd Versions) http://www.ktr.mlit.go.jp/omiya/04data/kisha/h22.htm
Tohoku Regional Development Bureau Iwate River and National Road Office	Earthquake Information : Iwate River and National Road Office (2nd and 3rd Versions) http://www.thr.mlit.go.jp/iwate/bousai/bousai/index.htm	Kanto Regional Development Bureau Shuto National Road Office	Damage of National Road No. 298 (18:50 on March 11) http://www.ktr.mlit.go.jp/syuto/index.htm
Tohoku Regional Development Bureau Sanriku National Road Office	Sanriku National Road Office Earthquake Information (2nd Version) http://www.thr.mlit.go.jp/sanriku/index.html	Kanto Regional Development Bureau Yokohama National Road Office	Damage Information in the 2011 off the Pacific Coast of Tohoku Earthquake (3rd Version) http://www.ktr.mlit.go.jp/yokohama/report/bn2010.htm
Tohoku Regional Development Bureau Sendai River and National Road Office	【Disaster Prevention Information】(Press Release) Sendai River and National Road Office Disaster Information (3rd, 13th, and 14th Versions) http://www.thr.mlit.go.jp/sendai/index.html	Aomori Prefecture	Disaster Countermeasures Office About the Damage in the 2011 off the Pacific Coast of Tohoku Earthquake (43th Version) http://www.pref.aomori.lg.jp/
Tohoku Regional Development Bureau Yamagata River and National Road Office	【Disaster Prevention Information】 Yamagata River and National Road Office Earthquake Information (3rd, 4th, 6th, and 7th Versions) http://www.thr.mlit.go.jp/bumon/kisya/saigai/sback/zokuhou1106.htm	Iwate Prefecture	Situation of Road Traffic Regulation Management due to the Earthquake in Iwate Prefecture on March 11 (As of 9:30 on August 12) http://www.pref.iwate.jp/list.rbz?nd=2974&ik=1&pnp=2974&of=13
Tohoku Regional Development Bureau Fukushima River and National Road Office	【Disaster Prevention Information】Fukushima River and National Road Office Earthquake Information (8th Version) http://www.thr.mlit.go.jp/fukushima/pressedit/disaster_index.html	Akita Prefecture	Information Earthquake (2nd, 4th, 5th, 6th, and 9th Versions) http://www.pref.akita.lg.jp/www/genre/000000000000/1243242791775/index.html
Tohoku Regional Development Bureau Koriyama National Road Office	【Disaster Prevention Information】 Koriyama National Road Office : Emergency System Response in the 2011 off the Pacific Coast of Tohoku Earthquake (2nd, 8th, and 20th Versions) http://www.thr.mlit.go.jp/bumon/kisya/saigai/sback/zokuhou1117.htm	Miyagi Prefecture	Traffic Regulation in the 2011 off the Pacific Coast of Tohoku Earthquake (As of 16:00 on May 8) http://www.pref.miyagi.jp/road/kiseinow.htm Damag of Public Facility and Emergency Disaster Recovery Situations in the 2011 off the Pacific Coast of Tohoku Earthquake (Updated August 10) http://www.pref.miyagi.jp/doboku/110311dbk_taiou/index.htm
Tohoku Regional Development Bureau Banryo National Road Office	【Disaster Prevention Information】 Banryo National Road Office : Road Disaster Prevention Information Earthquake (5th Version) http://www.thr.mlit.go.jp/bumon/kisya/saigai/sback/zokuhou1132.htm	Yamagata Prefecture	(Press Release) The 2011 off the Pacific Coast of Tohoku Earthquake (3rd and 10th Versions) http://www.pref.yamagata.jp/
Kanto Regional Development Bureau Main Office	Road Division at Kanto Regional Development Bureau Disaster Information of National Road in the 2011 off the Pacific Coast of Tohoku Earthquake (15:00 on March 18, 2011) http://www.ktr.mlit.go.jp/saigai/kyoku_dis00000021.html	East Nippon Expressway Company Limited	Damaged Routes and Sections (List) (March 18) http://www.e-nexco.co.jp/whatsnew/h22.html
Kanto Regional Development Bureau Hitachi River and National Road Office	Hitachi River and National Road Office (Press release) : Announcement for the Damage due to the 2011 off the Pacific Coast of Tohoku Earthquake (10:30 on March 12, 2011) http://www.ktr.mlit.go.jp/kisha/index00000022.html	Metropolitan Expressway Company Limited	(Press Release) Influence and Emergency Response due to the 2011 off the Pacific Coast of Tohoku Earthquake and Correspondence (March 14, 2011) http://www.shutoko.jp/
Kanto Regional Development Bureau Utsunomiya National Road Office	Road Damage Information for the 2011 off the Pacific Coast of Tohoku Earthquake (17:00 on March 11, 18:30 on March 11, 12:00 on March 12) http://www.ktr.mlit.go.jp/utunomiya/bousai/old.htm	—	—

clarifying the dependency of damage of road structures on occurrence of slope failures. Based on previous valuable results, we analyzed damage data on road structures due to slope failures in the 2011

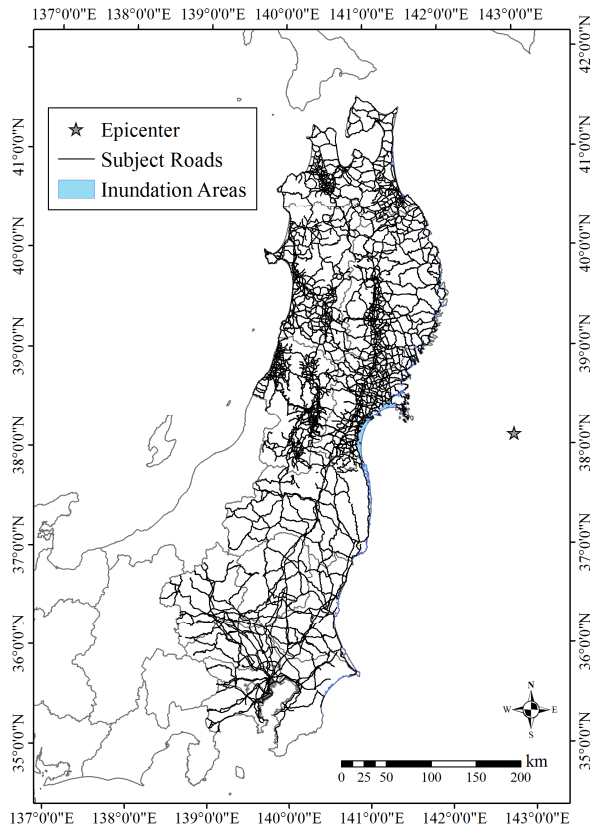


Fig. 1 Subject roads without inundation areas

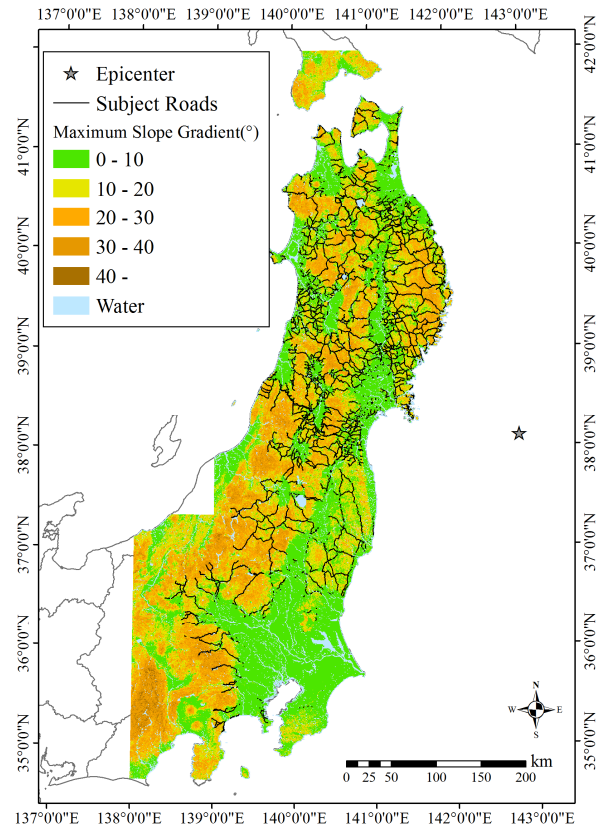


Fig. 2 Subject roads for analysis

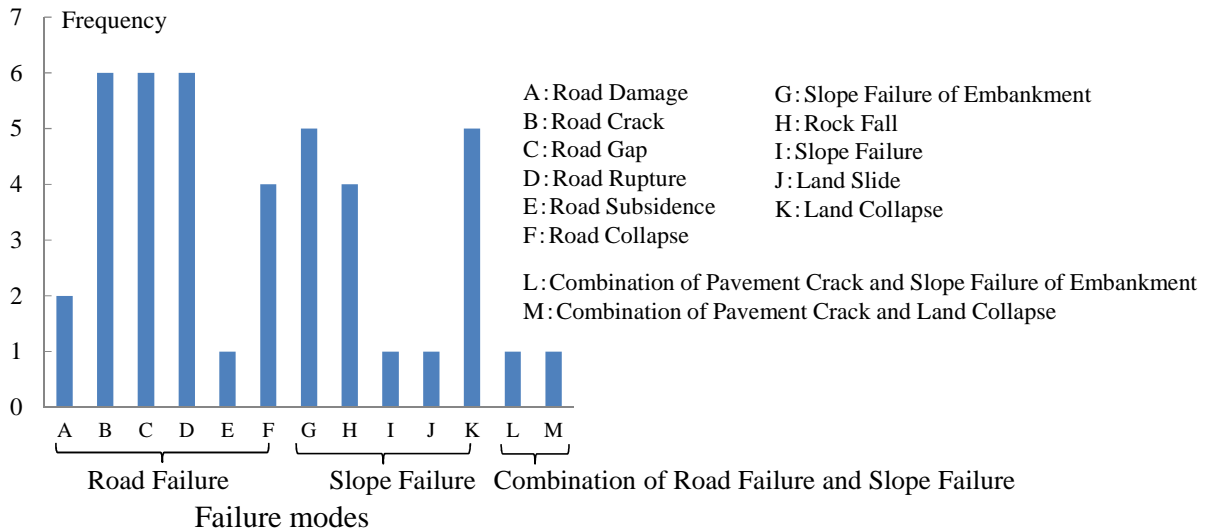


Fig. 3 Induced failure modes

off the Pacific Coast of Tohoku earthquake (hereinafter the Tohoku earthquake) and clarified the relationship of related damage ratios with spatial distributions of peak ground acceleration (*PGA*), peak ground velocity (*PGV*), and instrumental seismic intensity (*IJ*). In addition, damage functions on the failures of road structures due to slope failures in the 2008 Iwate-Miyagi Nairiku earthquake (hereinafter the Iwate-Miyagi Nairiku earthquake), proposed by Shoji and Sakurai (2011), are verified by comparing the derived results from this study with the values from the damage functions.

SUBJECT ROAD STRUCTURES AND THE DAMAGE MODES

Analyzed data of damaged road structures

Damage data of road structures due to slope failures except damage data of bridges and tunnels are analyzed. Analyzed road structures are national roads at six prefectures of Tohoku regions, Tokyo metropolitan areas and six prefectures of Kanto regions by Tohoku Regional Development Bureau, Kanto Regional Development Bureau, East Nippon Expressway Company Limited and Metropolitan Expressway Company Limited, and prefectural roads at five prefectures of Tohoku regions without Fukushima prefecture by local government sectors. Table 1 shows the information of damaged road structures which is opened at the related web sites by road management authorities and local government sectors. Total number of the data is 680. For selecting 680 data, we removed the damage data to be possibly affected by the ground motions due to the aftershocks after March 11, 2011.

Based on the data, first, we identified the locations of damaged road structures. Second, we removed 158 data as the data subjected to the tsunami waves by comparing the locations of damaged road structures with estimated inundation areas by GSI (2011) and selected 522 data as those dominantly exposed by the ground excitations.

Among 522 data, the exact locations of 360 data offered by East Nippon Expressway Company Limited cannot be clarified since these data show the number of damage points between any interchanges. Therefore, we removed above 360 data and set 162 data as analyzed ones. For 162 data, finally we focused on 43 data which are assumed to be affected by slope failures in subject areas showing maximum slope gradients equal to or over 10 degrees (Ishide and Yamazaki 2010). Furthermore, in order to verify validness of occurrence of slope failures and induced damage at subject road structures, we check all image data for 43 data by Google Earth.

We model subjected roads without estimated inundation areas by GSI as shown in Fig. 1, by using the digital data of national roads and major prefectural roads in 6 prefectures of Tohoku regions, Tokyo Metropolitan areas and 6 prefectures of Kanto regions offered by National and Regional Planning Bureau (2011) and by constructing the digital data of other prefectural roads in 5 prefectures of Tohoku regions except Fukushima prefecture by checking Google Earth. In addition, among above roads, we select the roads with slopes showing maximum slope gradients equal to or over 10 degrees as shown in Fig. 2. Again we checked the locations of roads with slopes by Google Earth. Total length of subject roads is 14,258km.

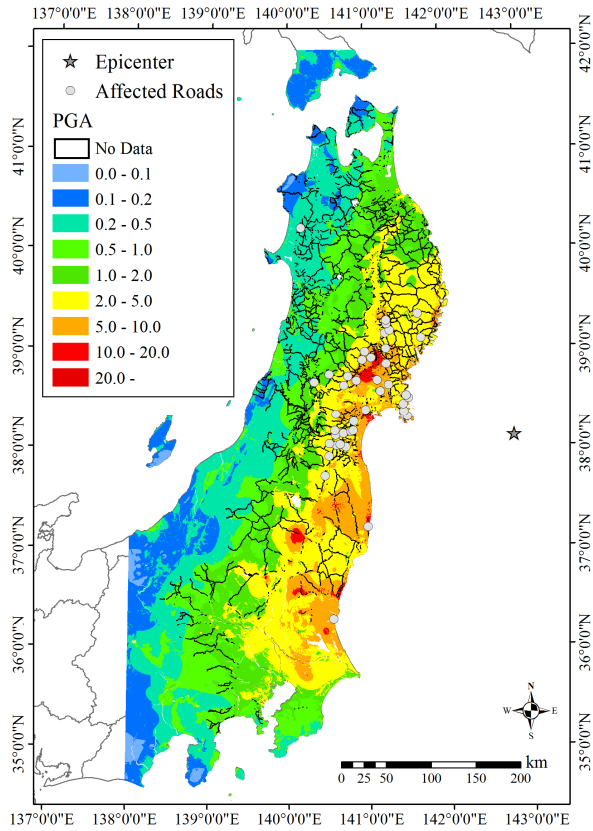
Damage modes

Fig. 3 shows 13 failure modes: 6 road failure modes, 5 slope failure modes, and 2 combination failure modes of road failure and slope failure. 25 data on road failure modes are classified into 6 failure modes: 6 data for road crack, 6 data for road gap, 6 data for road rupture, 4 data for road collapse, and others. 16 data on slope failure modes are classified into 5 failure modes: 5 data for failure of embankment slope, 5 data for land collapse, 4 data for rock fall, and others.

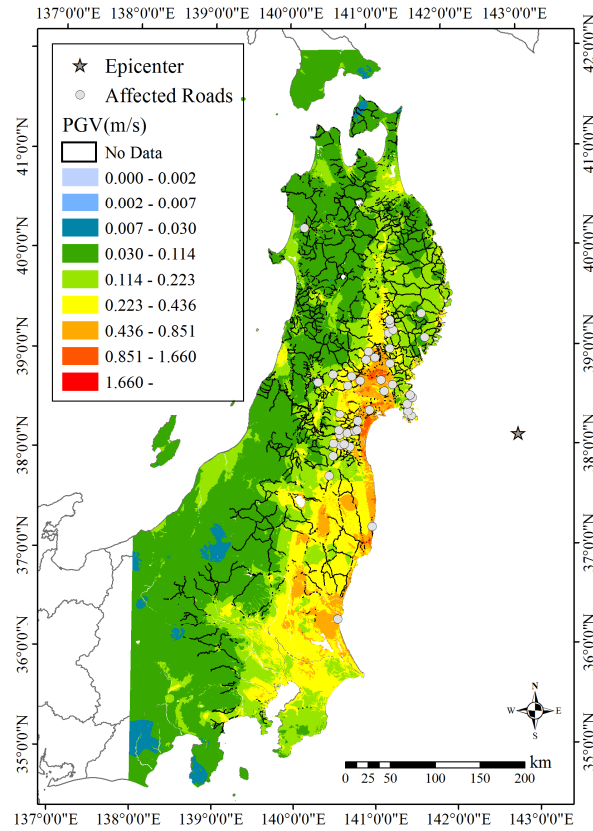
DAMAGE ASSESMENT FOR SUBJECT ROAD STRUCTURES

Evaluation of spatial distributions of *PGA*, *PGV*, and *IJ*

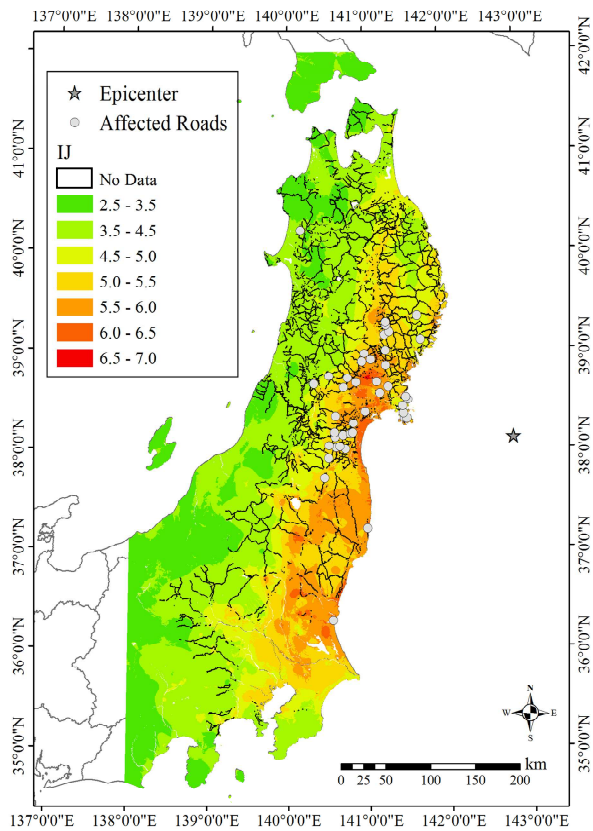
Fig. 4 shows estimated spatial distributions with a 250m-mesh of *PGA*, *PGV*, and *IJ* for analysis, based on the simple kriging method by using 535 observation waveforms by K-NET and KiK-net (NIED 2011), and 44 observation waveforms by JMA (2011b) as shown in Fig. 5. These observatory stations are distributed at Aomori, Akita, Yamagata, Iwate, Miyagi, Fukushima, Ibaraki, Tochigi, Gunma, Chiba, Saitama, Yamanashi, Nagano, and Niigata prefectures, and Tokyo Metropolitan areas. We describe the procedures of computing the distributions of *PGA*, *PGV*, and *IJ* in the followings.



(a) PGA distribution



(b) PGV distribution



(c) IJ distribution

Fig. 4 Spatial distributions of affected roads and *PGA*, *PGV*, and *IJ*

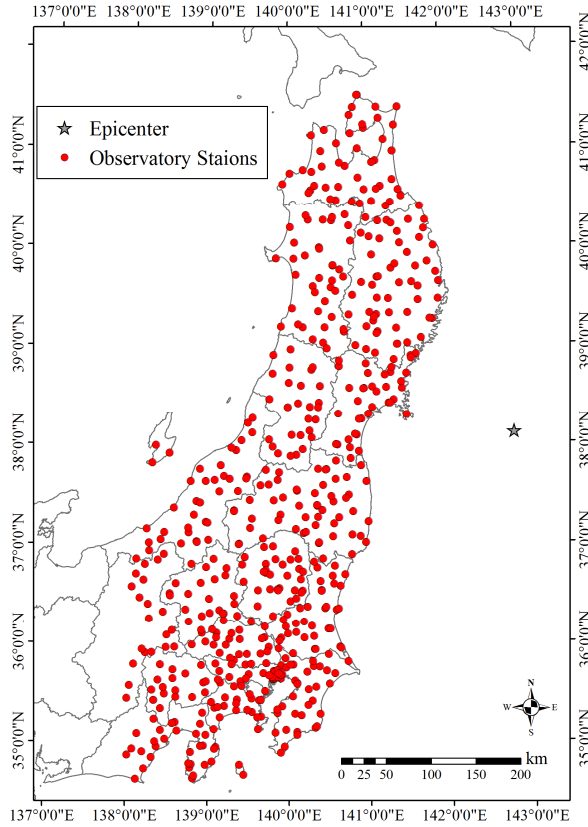


Fig. 5 Observatory stations for analysis

First, PGA at an arbitrary station is computed by selecting maximum value in a time history composing EW, NS, and UD components of an observed waveform. We calibrate the time history data by subtracting mean value from the data recorded by K-NET and KiK-net. We compute PGA_{b600} at a base level with average S wave velocity V_s of 600m/s by applying the related factors α , β on amplification of PGA at a ground surface compared with PGA_{b600} . The amplification factors α , β are obtained by the following equations proposed by Suetomi et al. (2005),

$$\left. \begin{aligned}
 X_s &= \alpha \cdot X_b && (X_b \leq X_1) \\
 X_s &= X_L - \beta \cdot (X_b - X_2) && (X_1 < X_b < X_2) \\
 X_2 &= \frac{2}{\alpha} X_L - X \\
 \beta &= \frac{X_L - \alpha \cdot X_1}{(X_2 - X_1)^2} \\
 X_s &= X_L && (X_b \geq X_2)
 \end{aligned} \right\} (1)$$

$$\log(\alpha) = 2.024 - 0.75 \cdot \log(AVS20) \quad (2)$$

$$\log(X_1) = 1.4 \cdot \log(AVS20) - 0.8 \quad (3)$$

$$\log(X_L) = 1.0 \cdot \log(AVS20) + 0.778 \quad (4)$$

Now, in Eq. (1) to Eq. (4), we set $X_s=PGA$ and $X_b=PGA_{b600}$, and interpret X_1 and X_2 as the threshold values describing the relation between X_s and X_b dependent on classification of subject ground condition. $AVS20$ is an average S wave velocity at a layer of 20m under a ground surface, and computed by the following equation proposed by Kanno et al. (2006),

$$AVS30 = 1.13AVS20 + 19.5 \quad (5)$$

where $AVS30$ is similarly average S wave velocity at a layer of 30m under a ground surface, and we obtain the value with a 250m-mesh from the data of geomorphologic classification (Matsuoka et al. 2005). By using estimated PGA_{b600} data at observatory stations, we compute PGA_{b600} with a 250m-mesh based on simple kriging interpolation. We use attenuation relationship between PGA_{b600} and minimum distance from an arbitrary site to a fault plate R proposed by Shi and Midorikawa (1999), for evaluating the mean trend component in adopting simple kriging method as shown in the following equation,

$$\text{Log}_{10}PGA_{b600} = c_1 - \text{Log}_{10}(R + c_2) + c_3 \quad (6)$$

where c_1 , c_2 , and c_3 are recurrence constants obtained by the least squares method. In addition, for evaluating the variance in adopting simple kriging method, we use exponential model as a covariance model,

$$\gamma = \text{Var}[PGA_{b600}^2] \exp(-h/a) \quad (7)$$

where γ is the covariance of PGA_{b600} , h is the distance between an arbitrary site with a 250m-mesh and the observatory station, and a is the correlation distance. We set $a=40\text{km}$ for which the variation of spatial distributions of PGA converges when a varies for 20km, 30km, 40km, and 50km.

PGV at an arbitrary station is computed by selecting maximum value in a time history composing two horizontal EW and NS components of an observed waveform integrated by acceleration EW and NS waveforms with filtering by Bata Worth high pass filter with lowest cut-off frequency of 0.05Hz and pass frequency of 0.1Hz for K-NET and KiK-net waveforms, and with filtering of cut-off frequency equal to or less than 0.2Hz by using the integration recurrence formula for JMA waveforms. We compute PGV_{b600} at a base level with average S wave velocity V_s of 600m/s by applying the related factor ARV on amplification of PGV at a ground surface compared with PGV_{b600} . The relation of PGV_{b600} with PGV is obtained by the following equations proposed by Fujimoto and Midorikawa (2006),

$$PGV_{b600} = PGV / ARV \quad (8)$$

$$\text{Log}_{10}ARV = 2.367 - 0.852\text{Log}_{10}AVS30 \quad (9)$$

By using estimated PGV_{b600} data at observatory stations, we compute PGV_{b600} with a 250m-mesh based on simple kriging interpolation. We use attenuation relationship between PGV_{b600} and R proposed by Shi and Midorkawa (1999), for evaluating the mean trend component in adopting Simple Kriging method as well as for computation of PGA . In addition, for evaluating the variance in adopting simple kriging method, we use exponential model as a covariance model. We set $a=40\text{km}$ for which the variation of spatial distribution of PGV converges when a varies for 20km, 30km, 40km, and 50km.

IJ at an arbitrary station is computed by computational scheme by JMA (2011c). We compute IJ_{b600} at a base level with average S wave velocity V_s of 600m/s by applying the related factors α , β on amplification of IJ at a ground surface compared with IJ_{b600} . The amplification factors α , β are obtained by the following equations proposed by Suetomi et al. (2005),

$$\left. \begin{aligned}
\lambda_{IJ} &= \alpha_{IJ} && (IJ_b \leq IJ_1) \\
\lambda_{IJ} &= \alpha_{IJ} - \beta \cdot (IJ_b - IJ_1) && (IJ_1 < IJ_b < IJ_2) \\
\beta_{IJ} &= \frac{\alpha_{IJ} - IJ_L + IJ_2}{IJ_2 - IJ_1} && \\
\lambda_{IJ} &= IJ_L - IJ_b && (IJ_2 \leq IJ_b)
\end{aligned} \right\} (10)$$

$$\alpha_{IJ} = 2.699 - \log(AVS20) \quad (11)$$

$$IJ_1 = 0.8 + 2.25 \cdot \log(AVS20) \quad (12)$$

$$IJ_2 = 1.15 + 2.4 \cdot \log(AVS20) \quad (13)$$

$$IJ_L = 2.2 + 2.0 \cdot \log(AVS20) \quad (14)$$

By using estimated IJ_{b600} data at observatory stations, we compute IJ_{b600} with a 250m-mesh based on simple kriging interpolation. We apply same procedures for evaluating the mean trend component and variance in adopting simple kriging method, and for setting the correlation distance a as well as the procedures for computation of spatial distributions of PGA and PGV .

We verify the derived spatial distributions of PGA , PGV , and IJ from above procedures with same spatial distributions computed by NIED (2011), JMA (2011a), Suetomi and Fukushima (2011), and AIST (2011), and we check the agreement of our results with the reference results.

Relations of damage ratio with PGA , PGV , and IJ

Fig. 6 shows the relations between road damage and spatial distributions of PGA , PGV , and IJ . Now, we define damage ratio R as the ratio of the number of damage points X divided by total exposed road lengths L in an unit of kilometer. For damage ratio R with PGA of 0m/s^2 to 20m/s^2 , the interval of PGA is set as 0.5m/s^2 , for R with PGV of 0.01m/s to 1.4m/s , the interval of PGV is set as 0.01m/s , and for R with IJ of 2.5 to 6.7 , the interval of IJ is set as 0.1 .

From Fig. 6(a), R with PGA of 0.5m/s^2 shows the minimum value of $0.000264/\text{km}$ at the lowest limit of PGA and R with PGA of 11.5m/s^2 shows the maximum value of $0.0589/\text{km}$. R with PGA of 1.5m/s^2 to 3.0m/s^2 increases the value of $0.000637/\text{km}$ to $0.00333/\text{km}$, R with PGA of 3.0m/s^2 to 7.0m/s^2 increases the value of $0.00264/\text{km}$ to $0.0316/\text{km}$, and R with PGA of 9.0m/s^2 to 11.5m/s^2 increases the value of $0.0229/\text{km}$ to $0.0589/\text{km}$. In contrast, R with PGA over 12m/s^2 shows zero in spite of becoming higher PGA . This is because the possibility of occurrence of road damage becomes low with shortening exposed road lengths less than 17.7km .

From Fig. 6(b), R with PGV of 0.1m/s shows the minimum value of $0.00239/\text{km}$ at the lowest limit of PGV and R with PGV of 0.62m/s shows the maximum value of $0.0687/\text{km}$. R with PGV of 0.1m/s to 0.3m/s increases the value of $0.00239/\text{km}$ to $0.0202/\text{km}$, R with PGV of 0.3m/s to 0.5m/s increases the value of $0.00964/\text{km}$ to $0.0508/\text{km}$, and R with PGV of 0.5m/s to 0.62m/s increases the value of $0.0312/\text{km}$ to $0.0687/\text{km}$. R with PGV over 0.63m/s shows zero in spite of becoming higher PGV , that is caused by same reason for higher PGA over 12m/s^2 .

From Fig. 6(c), R with IJ of 3.7 shows the lower value of $0.00169/\text{km}$ at the lowest limit of IJ and R with IJ of 5.9 shows the maximum value of $0.0226/\text{km}$. R with IJ of 4.5 to 5.0 increases the value of $0.00176/\text{km}$ to $0.00401/\text{km}$, R with IJ of 5.0 to 5.5 increases the value of $0.00157/\text{km}$ to $0.0139/\text{km}$, and R with IJ of 5.5 to 5.9 increases the value of $0.00690/\text{km}$ to $0.0226/\text{km}$. Similarly, R with IJ over 6.0 shows zero in spite of becoming higher IJ .

Comparison of analyzed data with previous damage functions

Fig. 7 shows the comparison of analyzed data for the Tohoku earthquake with damage ratios for the Iwate-Miyagi Nairiku earthquake data and damage functions by the Iwate-Miyagi Nairiku earthquake data proposed by Shoji and Sakurai (2011).

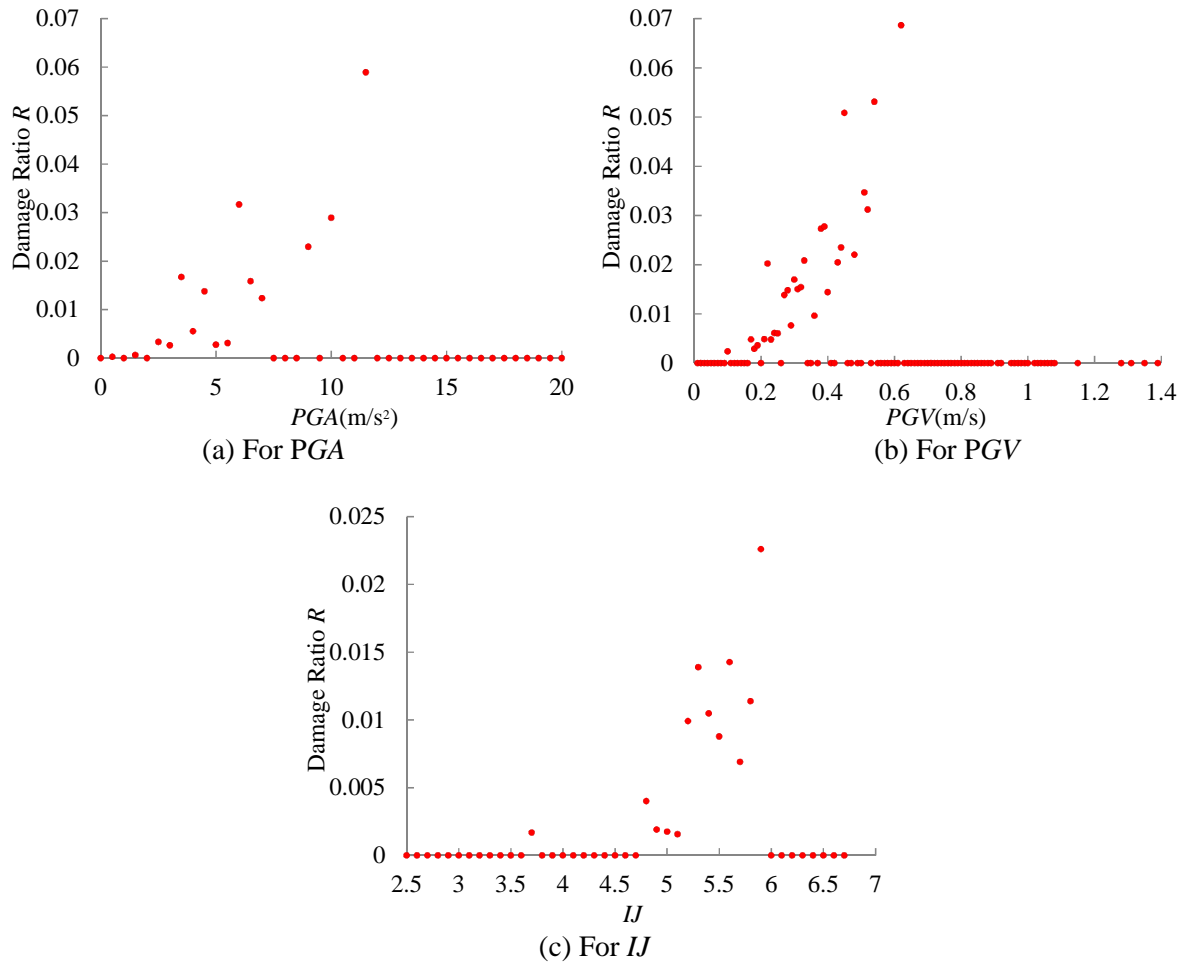


Fig. 7 Comparison of the damage ratio for PGA , PGV , and IJ

From Fig. 7(a), averaged values of difference from observed data for the Iwate-Miyagi Nairiku earthquake to analyzed data for the Tohoku earthquake with PGA of $3.0m/s^2$ to $6.0m/s^2$ shows $0.038/km$ and those with PGA of $6.0m/s^2$ to $10m/s^2$ at higher PGA becomes the larger value of $0.13/km$. Averaged values of difference from the values by damage function to analyzed data for the Tohoku earthquake with PGA of $3.0m/s^2$ to $6.0m/s^2$ shows $0.036/km$ and those with PGA of $6.0m/s^2$ to $10m/s^2$ at higher PGA shows the larger value of $0.18/km$. In the above, R with relatively lower PGA of $3.0m/s^2$ to $6.0m/s^2$ shows the narrow differences. In contrast, R with relatively higher PGA of $6.0m/s^2$ to $10m/s^2$ shows the wider differences.

From Fig. 7(b), averaged values of difference from observed data for the Iwate-Miyagi Nairiku earthquake to analyzed data for the Tohoku earthquake with PGV of $0.1m/s$ to $0.3m/s$ shows $0.052/km$ and those with PGV of $0.5m/s$ to $0.6m/s$ shows the larger value of $0.22/km$. Averaged values of difference from the values by damage function to analyzed data for the Tohoku earthquake with PGV of $0.1m/s$ to $0.3m/s$ shows $0.0043/km$ and those with PGV of $0.5m/s$ to $0.6m/s$ shows the larger of $0.17/km$. In the above, R with relatively lower PGV of $0.1m/s$ to $0.3m/s$ shows the narrow differences. In contrast, R with relatively higher PGV of $0.5m/s$ to $0.6m/s$ shows the larger wider differences.

From Fig. 7(c), averaged values of difference from observed data for the Iwate-Miyagi Nairiku earthquake to analyzed data for the Tohoku earthquake with IJ of 4.5 to 5.5 shows $0.024/km$ and those with IJ of 5.5 to 6.5 shows the larger value of $0.26/km$. Averaged values of difference from the values by damage function to analyzed data for the Tohoku earthquake with IJ of 4.5 to 5.5 shows $0.017/km$ and those with IJ of 5.5 to 6.5 shows the larger value of $0.29/km$. In the above, R with relatively lower IJ of 4.5 to 5.5 shows the narrow differences. In contrast, R with relatively higher IJ of 4.5 to 5.5 shows the larger wider differences.

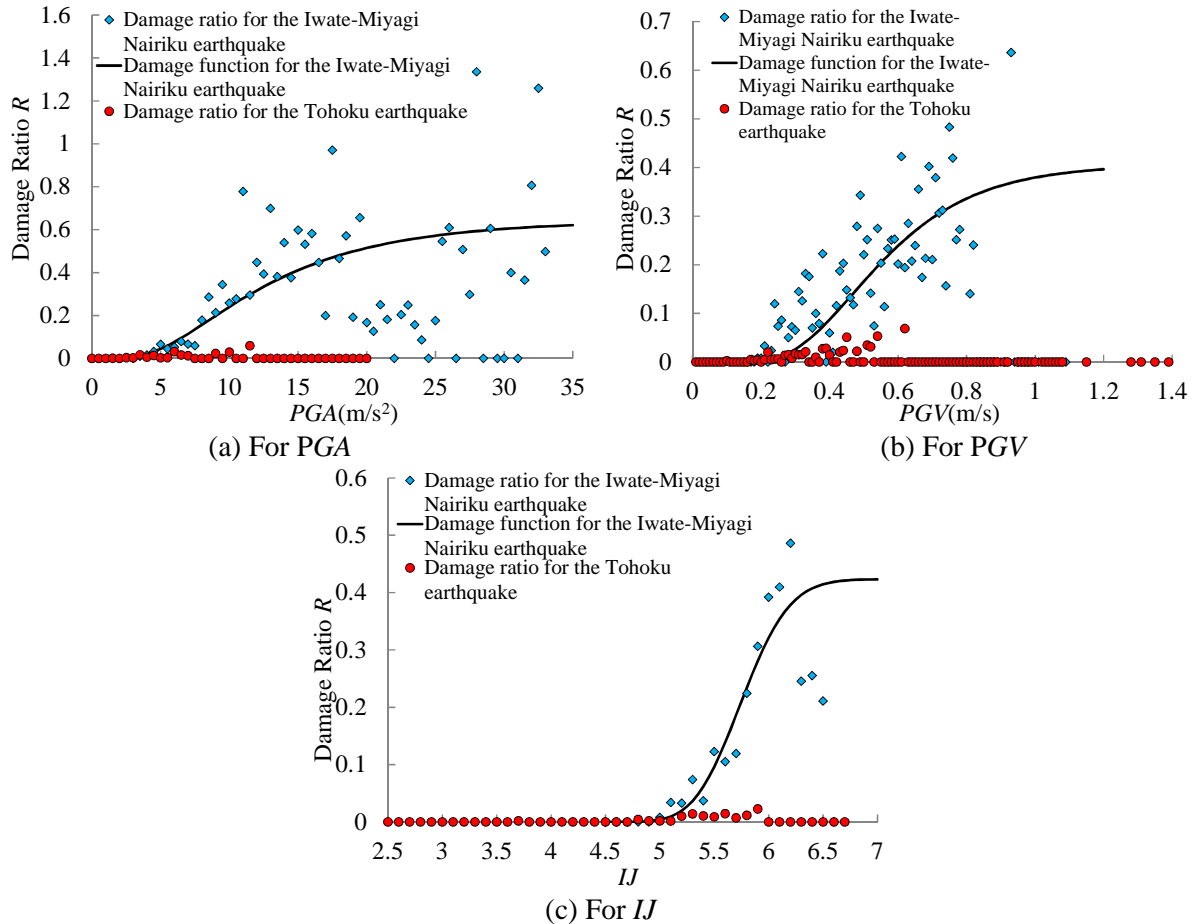


Fig. 6 Comparison of analyzed data for the Tohoku earthquake with damage ratios for the Iwate-Miyagi Nairiku earthquake data and damage functions by the Iwate-Miyagi Nairiku earthquake data

Hence, ground excitations with PGA of 6.0m/s^2 to 10m/s^2 , PGV of 0.5m/s to 0.6m/s , and IJ of 4.5 to 5.5 for the Iwate-Miyagi Nairiku earthquake induced larger damage of road structures due to slope failures than those with same ranges of PGA , PGV , and IJ for the Tohoku earthquake.

CONCLUSIONS

We analyzed damage data on road structures due to slope failures in the 2011 off the Pacific Coast of Tohoku earthquake and clarified the relationship of related damage ratios with spatial distributions of peak ground acceleration (PGA), peak ground velocity (PGV), and instrumental seismic intensity (IJ). In addition, previously proposed damage functions on the failures of road structures due to slope failures in the 2008 Iwate-Miyagi Nairiku earthquake are verified by comparing the derived results from this study with the values from the damage functions.

- (1) The failure modes are classified for 43 data on the damage of road structures due to slope failures into 13 failure modes: 6 road failure modes, 5 slope failure modes, and 2 combination failure modes of road failure and slope failure. 25 data on road failure modes are classified into 6 failure modes: 6 data for road crack, 6 data for road gap, 6 data for road rupture, 4 data for road collapse, and others. 16 data on slope failure modes are classified into 5 failure modes: 5 data for failures of embankment slope, 5 data for land collapse, 4 data for rock fall, and others.
- (2) Damage ratio R was defined as the ratio of the number of damage points X divided by total exposed road lengths L in an unit of kilometer. R with PGA of 0.5m/s^2 shows the minimum value of $0.000264/\text{km}$ at the lowest limit of PGA and R with PGA of 11.5m/s^2 shows the maximum value

of 0.0589/km. R with PGV of 0.1m/s shows the minimum value of 0.00239/km at the lowest limit of PGV and R with PGV of 0.62m/s shows the maximum value of 0.0687/km. R with IJ of 3.7 shows the lower value of 0.00169/km at the lowest limit of IJ and R with IJ of 5.9 shows the maximum value of 0.0226/km.

- (3) Ground excitations with PGA of 6.0m/s² to 10m/s², PGV of 0.5m/s to 0.6m/s, and IJ of 4.5 to 5.5 for the Iwate-Miyagi Nairiku earthquake induced larger damage of road structures due to slope failures than those with same ranges of PGA , PGV , and IJ for the Tohoku earthquake.

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